

## ATL43xx 2.5V Low Iq Adjustable Precision Shunt Regulator

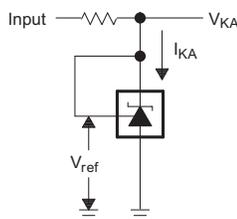
### 1 Features

- Adjustable Regulated Output of 2.5 V to 36 V
- Very low operating current
  - $I_{KA(min)} = 35 \mu\text{A}$  (max)
  - $I_{REF} = 150 \text{ nA}$  (max)
- Internally Compensated for Stability
  - Stable with no capacitive load
- Reference Voltage Tolerances at 25°C
  - 0.5% for ATL43xB
  - 1% for ATL43xA
- Typical Temperature Drift
  - 5 mV (–40°C to 85°C) ; "I" version
  - 6 mV (–40°C to 125°C); "Q" version
- Extended Cathode Current Range 35  $\mu\text{A}$  to 100 mA
- Low Output Impedance of 0.3  $\Omega$  (max)
- ATL431AQ, ATL431BI, ATL431BQ Are Currently In Preview
- ATL432AI, ATL432AQ, ATL432BI, ATL432BQ Are Currently In Preview

### 2 Applications

- Secondary Side Regulation in Flyback SMPSs
- Industrial, Computing, Consumer & Portables
- Adjustable Voltage and Current Referencing
- Power Management
- Power Isolation
- Zener Replacement

### 4 Simplified Schematic



### 3 Description

The ATL431 and ATL432 are three-terminal adjustable shunt regulators, with specified thermal stability over applicable automotive, commercial, and industrial temperature ranges. The output voltage can be set to any value between  $V_{ref}$  (approximately 2.5 V) and 36 V, with two external resistors. These devices have a typical output impedance of 0.05  $\Omega$ . Active output circuitry provides a very sharp turn-on characteristic, making these devices excellent replacements for Zener diodes in many applications, such as onboard regulation, adjustable power supplies, and switching power supplies.

The ATL43X has > 20x improvement Cathode current range over its TL43X predecessor. It also is stable with a wider range of load capacitance types and values.

ATL431 and ATL432 are the exact same parts but with different pinouts and order numbers. The ATL43X is offered in two grades, with initial tolerances (at 25°C) of 0.5%, 1%, for the B and A grade, respectively. In addition, low output drift vs temperature ensures good stability over the entire temperature range.

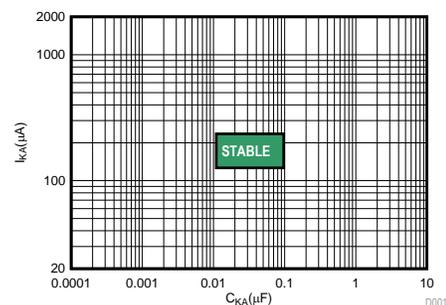
The ATL43xxI devices are characterized for operation from –40°C to 85°C, and the ATL43xxQ devices are characterized for operation from –40°C to 125°C.

#### Device Information<sup>(1)</sup>

PART NUMBER	PACKAGE	BODY SIZE (NOM)
ATL43x	SOT (3)	2.90 mm x 1.60 mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.

#### Stability Region for $V_{KA} = 15.0 \text{ V}$



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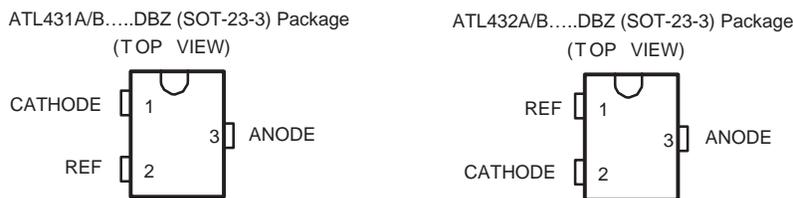
## 5 Revision History

### Changes from Original (March 2013) to Revision A

Page

• Initial release of full version .....	<b>1</b>
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## 6 Pin Configuration and Functions



### Pin Functions

NAME	PIN		I/O	DESCRIPTION
	NO.			
	ATL431x	ATL432x		
CATHODE	1	2	I/O	Shunt Current/Voltage input
REF	2	1	I	Threshold relative to common anode
ANODE	3	3	O	Common pin, normally connected to ground

## 7 Specifications

### 7.1 Absolute Maximum Ratings<sup>(1)</sup>

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
$V_{KA}$	Cathode voltage <sup>(2)</sup>		40	V
$I_{KA}$	Continuous cathode current range	-100	150	mA
$I_{I(ref)}$	Reference input current range	-0.05	10	mA
$T_J$	Operating virtual junction temperature	-40	150	°C
$T_{stg}$	Storage temperature range	-65	150	°C

- Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- All voltage values are with respect to ANODE, unless otherwise noted.

### 7.2 ESD Ratings

		VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000
		Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	±1000

- JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 7.3 Thermal Information

THERMAL METRIC <sup>(1)</sup>	ATL43xx		UNIT
	DBZ		
	3 PINS		
$\theta_{JA}$	Junction-to-ambient thermal resistance	331.8	°C/W
$\theta_{JCTop}$	Junction-to-case (top) thermal resistance	106.5	°C/W
$\theta_{JB}$	Junction-to-board thermal resistance	64.6	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	4.9	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	62.9	°C/W

- For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, [SPRA953](#).

## 7.4 Recommended Operating Conditions

		MIN	MAX	UNIT	
$V_{KA}$	Cathode voltage	$V_{ref}$	36	V	
$I_{KA}$	Cathode current	.035	100	mA	
$T_A$	Operating free-air temperature	"I" Grade	-40	85	°C
		"Q" Grade	-40	125	

## 7.5 Electrical Characteristics, ATL431Ax, ATL432Ax

 over recommended operating conditions,  $T_A = 25^\circ\text{C}$  (unless otherwise noted)

PARAMETER	TEST CIRCUIT	TEST CONDITIONS	ATL431Ax, ATL432Ax			UNIT	
			MIN	TYP	MAX		
$V_{ref}$	Reference voltage	Figure 23	$V_{KA} = V_{ref}, I_{KA} = 1\text{ mA}$			mV	
$V_{I(dev)}$	Deviation of reference input voltage over full temperature range, see <a href="#">Notes</a> section	Figure 23	$V_{KA} = V_{ref}, I_{KA} = 1\text{ mA}$	ATL43XA1; $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	5	15	mV
				ATL43XAQ; $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	6	34	
$\frac{\Delta V_{ref}}{\Delta V_{KA}}$	Ratio of change in reference voltage to the change in cathode voltage	Figure 24	$I_{KA} = 1\text{ mA}$	$\Delta V_{KA} = 10\text{ V} - V_{ref}$	-0.4	-2.7	mV/V
				$\Delta V_{KA} = 36\text{ V} - 10\text{ V}$	-0.1	-2	
$I_{ref}$	Reference input current	Figure 24	$I_{KA} = 1\text{ mA}, R1 = 10\text{ k}\Omega, R2 = \infty$			nA	
$I_{I(dev)}$	Deviation of reference input current over full temperature range, see <a href="#">Notes</a> section	Figure 24	$I_{KA} = 1\text{ mA}, R1 = 10\text{ k}\Omega, R2 = \infty$			nA	
$I_{min}$	Minimum cathode current for regulation	Figure 23 Figure 6	$V_{KA} = V_{ref}$			$\mu\text{A}$	
$I_{off}$	Off-state cathode current	Figure 25	$V_{KA} = 36\text{ V}, V_{ref} = 0$			$\mu\text{A}$	
$ z_{KA} $	Dynamic impedance, see <a href="#">Notes</a> section	Figure 23	$V_{KA} = V_{ref}, f \leq 1\text{ kHz}, I_{KA} = 1\text{ mA}$ to $100\text{ mA}$			$\Omega$	

## 7.6 Electrical Characteristics, ATL431Bx, ATL432Bx

 over recommended operating conditions,  $T_A = 25^\circ\text{C}$  (unless otherwise noted)

PARAMETER	TEST CIRCUIT	TEST CONDITIONS	ATL431Bx, ATL432Bx			UNIT	
			MIN	TYP	MAX		
$V_{ref}$	Reference voltage	Figure 23	$V_{KA} = V_{ref}, I_{KA} = 1\text{ mA}$			mV	
$V_{I(dev)}$	Deviation of reference input voltage over full temperature range, see <a href="#">Notes</a> section	Figure 23	$V_{KA} = V_{ref}, I_{KA} = 1\text{ mA}$	ATL43XB1; $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	5	15	mV
				ATL43XBQ; $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	6	34	
$\frac{\Delta V_{ref}}{\Delta V_{KA}}$	Ratio of change in reference voltage to the change in cathode voltage	Figure 24	$I_{KA} = 1\text{ mA}$	$\Delta V_{KA} = 10\text{ V} - V_{ref}$	-0.4	-2.7	mV/V
				$\Delta V_{KA} = 36\text{ V} - 10\text{ V}$	-0.1	-2	
$I_{ref}$	Reference input current	Figure 24	$I_{KA} = 1\text{ mA}, R1 = 10\text{ k}\Omega, R2 = \infty$			nA	
$I_{I(dev)}$	Deviation of reference input current over full temperature range, see <a href="#">Notes</a> section	Figure 24	$I_{KA} = 1\text{ mA}, R1 = 10\text{ k}\Omega, R2 = \infty$			nA	
$I_{min}$	Minimum cathode current for regulation	Figure 23 Figure 6	$V_{KA} = V_{ref}$			$\mu\text{A}$	
$I_{off}$	Off-state cathode current	Figure 25	$V_{KA} = 36\text{ V}, V_{ref} = 0$			$\mu\text{A}$	
$ z_{KA} $	Dynamic impedance, see <a href="#">Notes</a> section	Figure 23	$V_{KA} = V_{ref}, f \leq 1\text{ kHz}, I_{KA} = 1\text{ mA}$ to $100\text{ mA}$			$\Omega$	

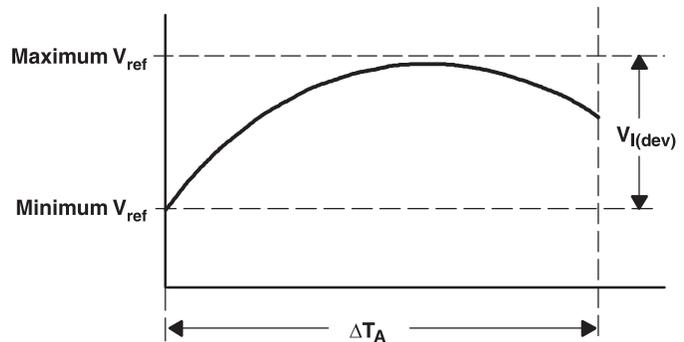
### 7.7 Notes

The deviation parameters  $V_{ref(dev)}$  and  $I_{ref(dev)}$  are defined as the differences between the maximum and minimum values obtained over the rated temperature range. The average full-range temperature coefficient of the reference input voltage  $\alpha_{Vref}$  is defined as:

$$|\alpha_{Vref}| \left( \frac{ppm}{^{\circ}C} \right) = \frac{\left( \frac{V_{I(dev)}}{V_{ref \text{ at } 25^{\circ}C}} \right) \times 10^6}{\Delta T_A}$$

where:

$\Delta T_A$  is the rated operating temperature range of the device.



$\alpha_{Vref}$  is positive or negative, depending on whether minimum  $V_{ref}$  or maximum  $V_{ref}$ , respectively, occurs at the lower temperature.

The dynamic impedance is defined as:  $|z_{KA}| = \frac{\Delta V_{KA}}{\Delta I_{KA}}$

When the device is operating with two external resistors (see [Figure 24](#)), the total dynamic impedance of the circuit is given by:  $|z'| = \frac{\Delta V}{\Delta I}$  which is approximately equal to  $|z_{KA}| \left( 1 + \frac{R1}{R2} \right)$

## 8 Typical Characteristics

Data at high and low temperatures are applicable only within the recommended operating free-air temperature ranges of the various devices.

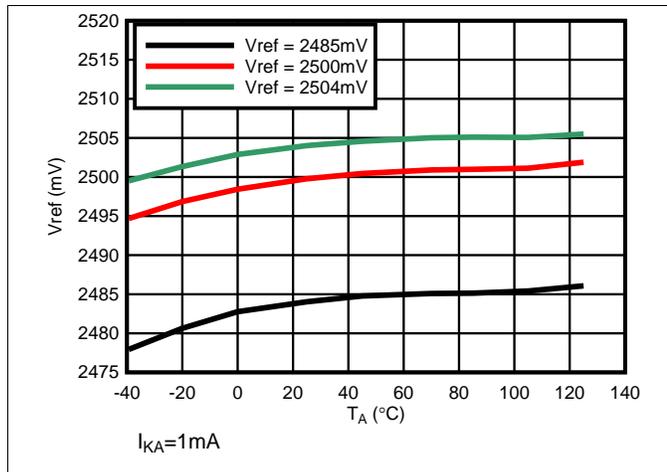


Figure 2. Reference Voltage vs Free-Air Temperature

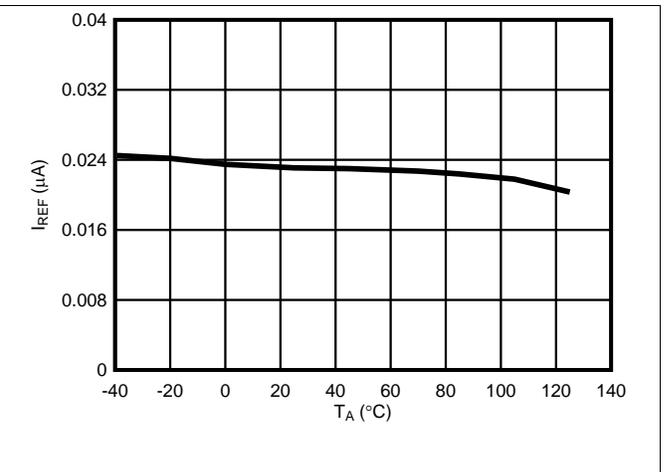


Figure 3. Reference Current vs Free-Air Temperature

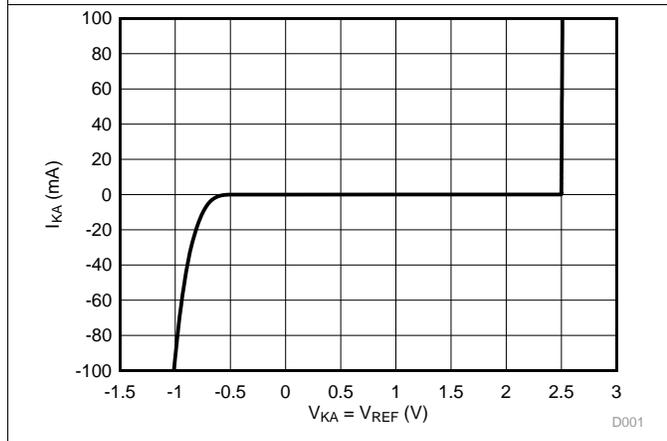


Figure 4. Cathode Current vs Cathode Voltage

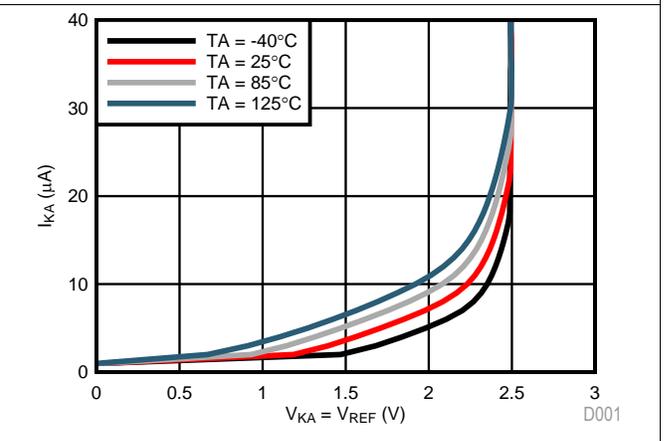


Figure 5. Cathode Current vs Cathode Voltage

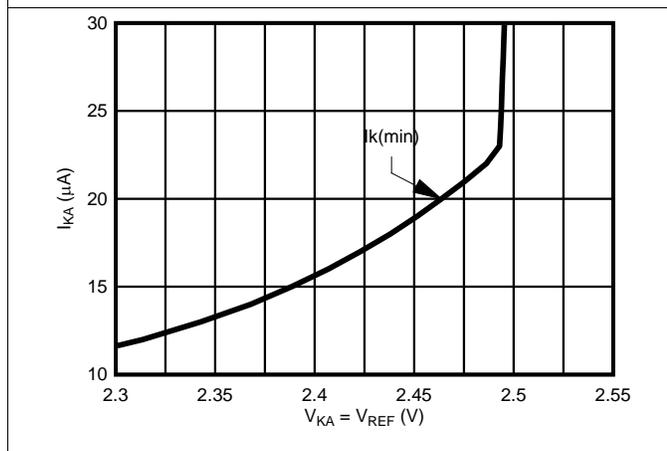


Figure 6. Cathode Current vs Cathode Voltage

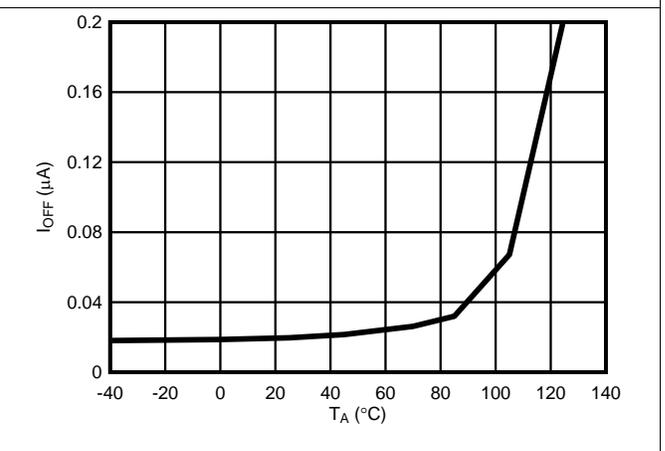
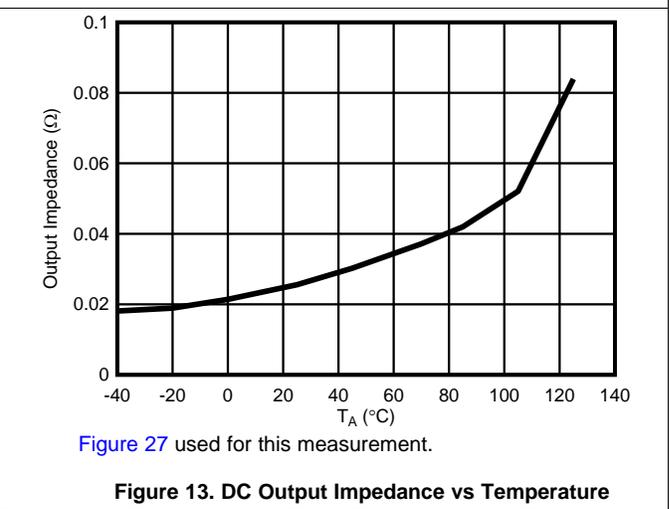
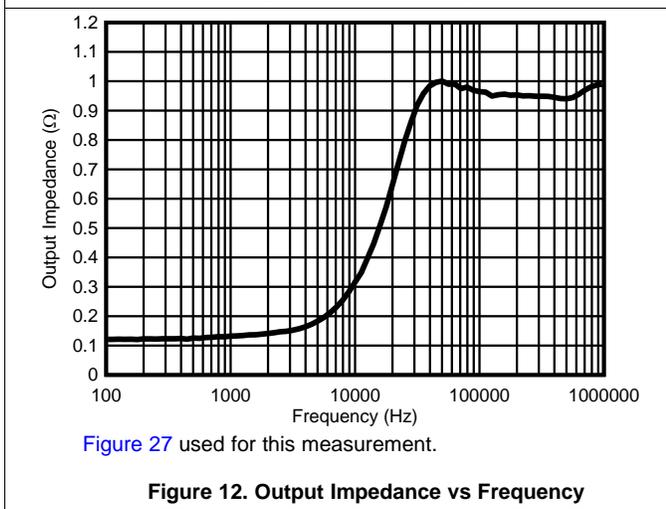
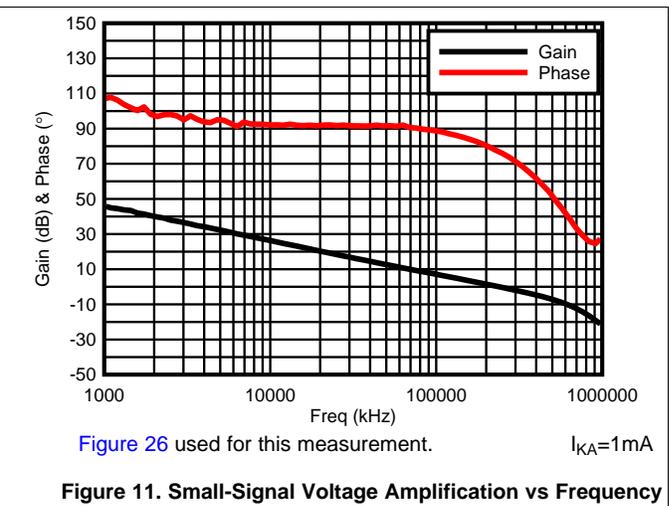
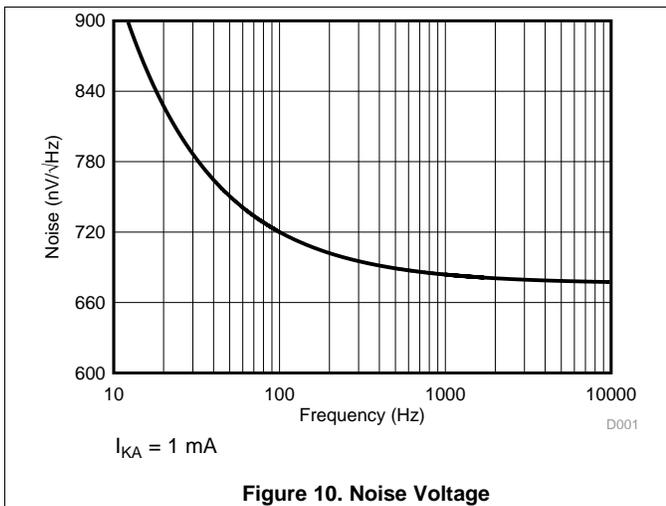
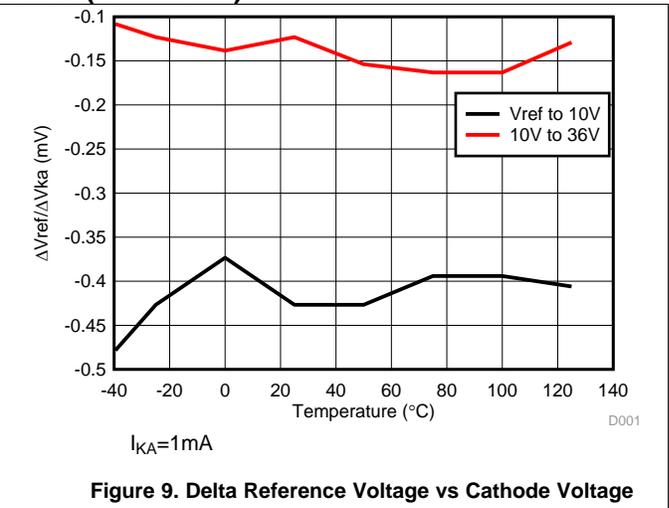
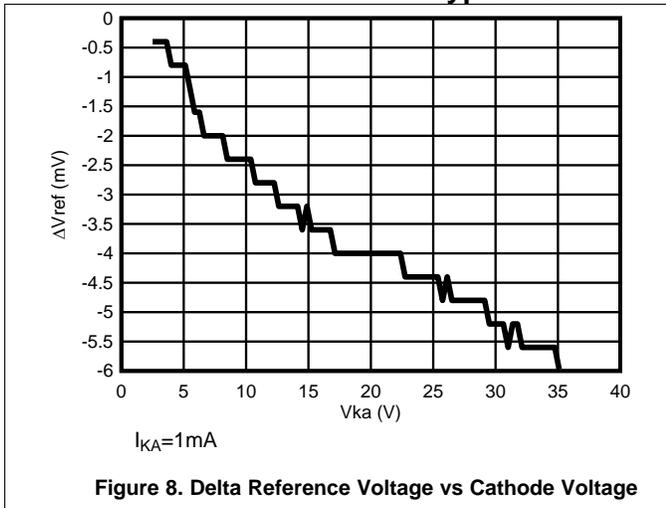
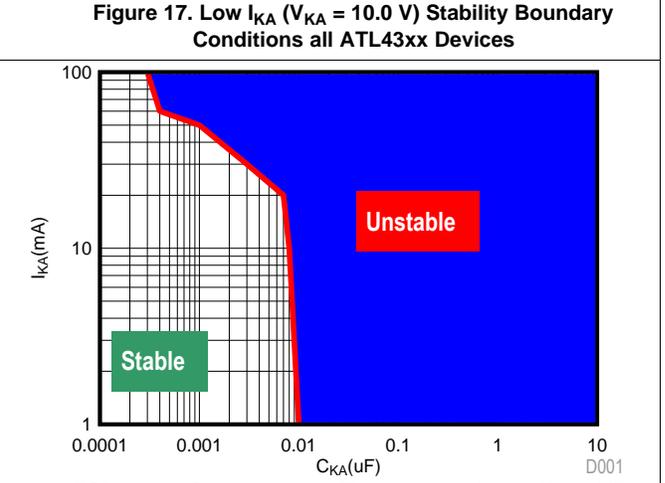
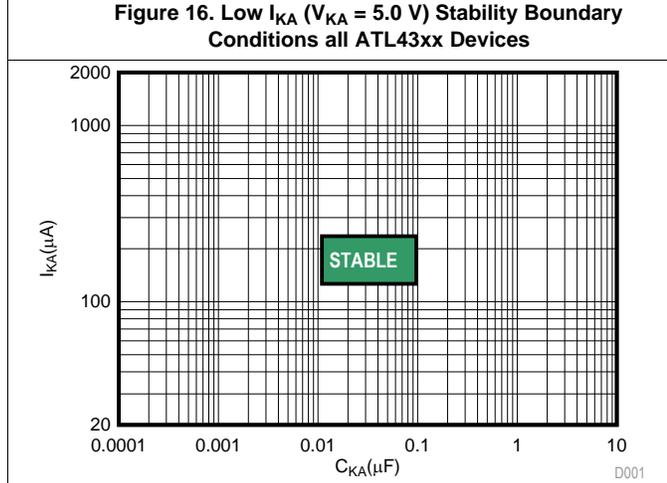
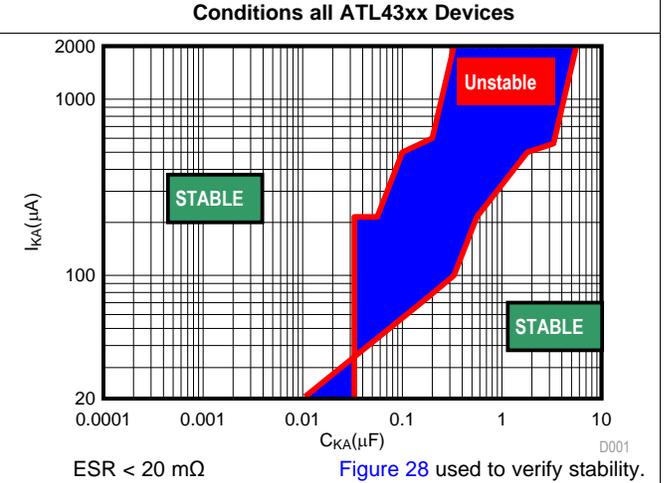
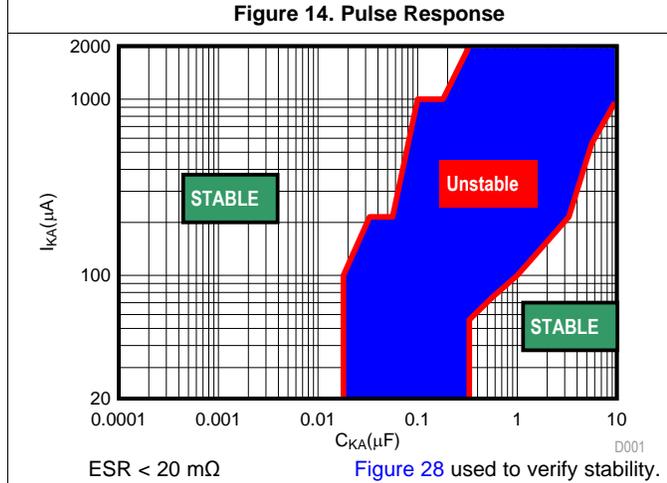
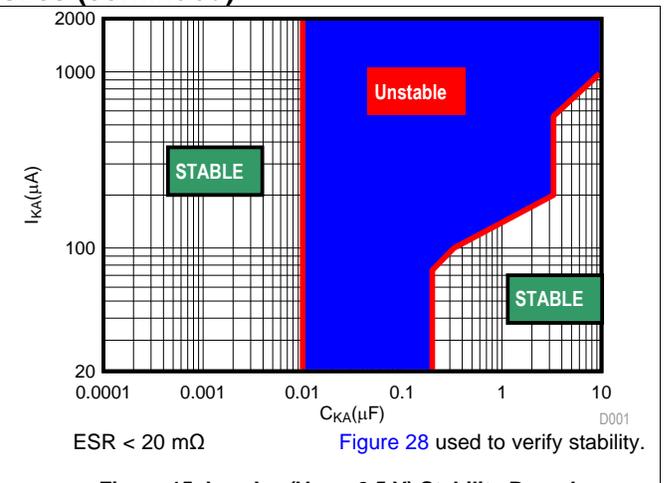
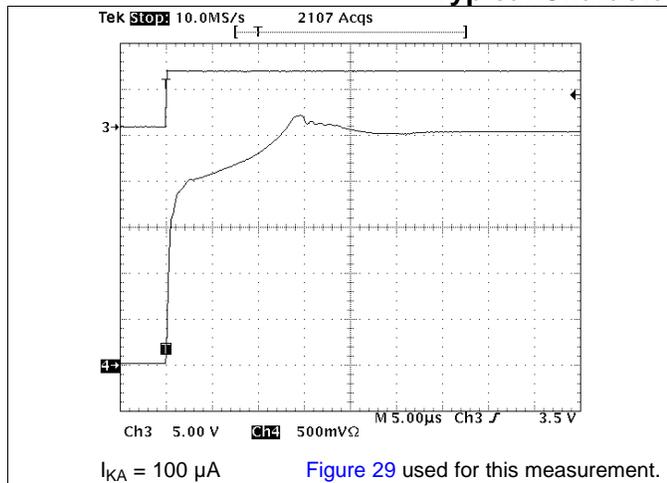


Figure 7. Off-State Cathode Current vs Free-Air Temperature

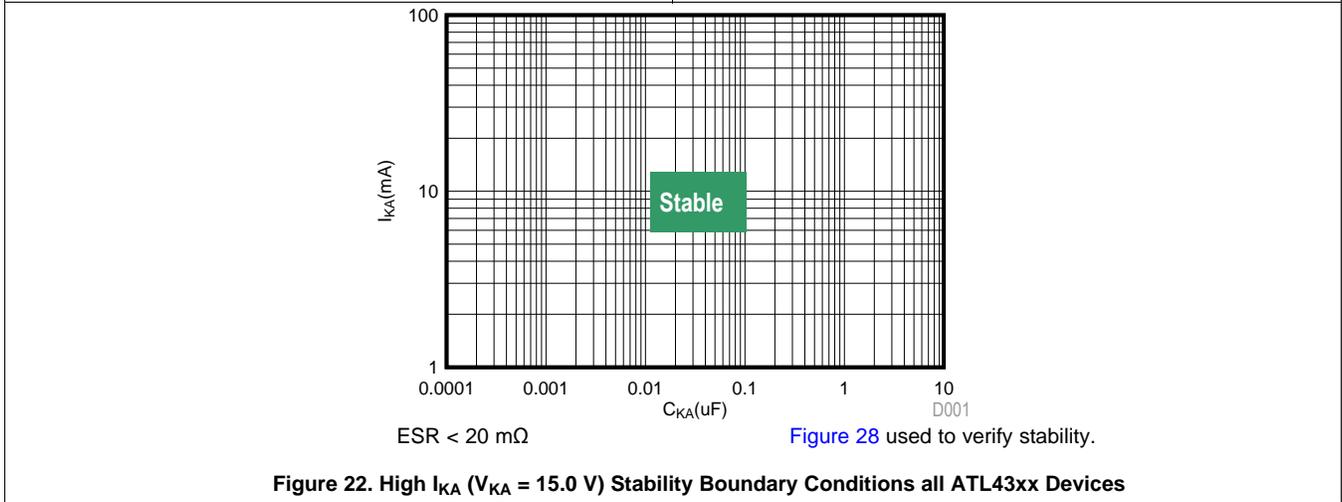
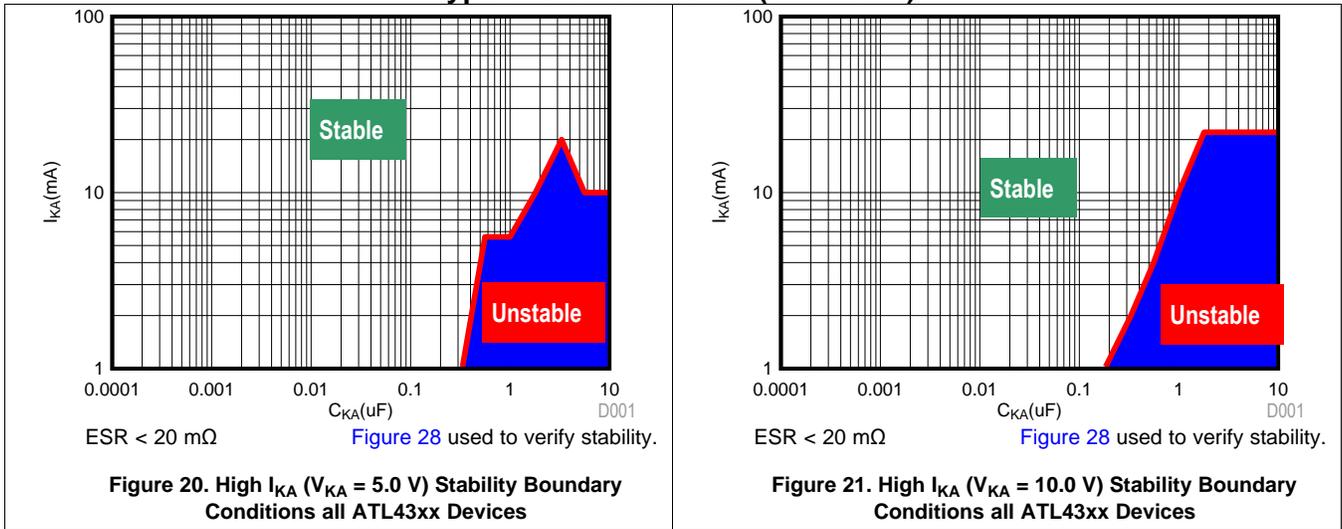
Typical Characteristics (continued)



Typical Characteristics (continued)



Typical Characteristics (continued)



## 9 Parameter Measurement Information

<p><b>Figure 23. Test Circuit for <math>V_{KA} = V_{ref}</math></b></p>	$V_{KA} = V_{ref} \left( 1 + \frac{R1}{R2} \right) + I_{ref} \times R1$ <p><b>Figure 24. Test Circuit for <math>V_{KA} &gt; V_{ref}</math></b></p>
<p><b>Figure 25. Test Circuit for <math>I_{off}</math></b></p>	<p><b>Figure 26. Test Circuit for Phase and Gain Measurement</b></p>
<p><b>Figure 27. Test Circuit for Reference Impedance (<math>Z_{KA}</math>)</b></p>	<p><b>Figure 28. Test Circuit for Stability Boundary Conditions</b></p>

Parameter Measurement Information (continued)

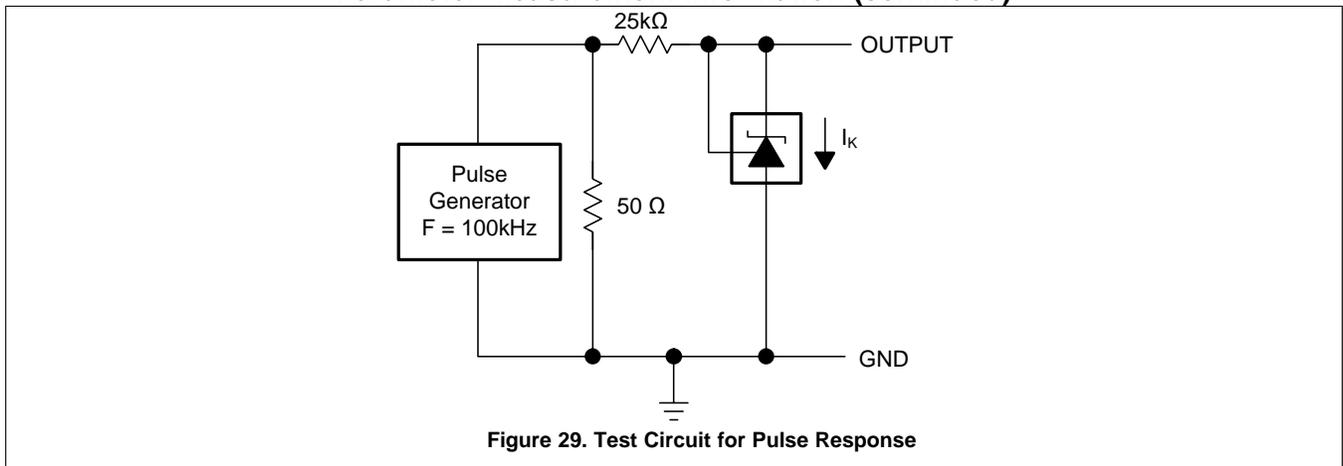


Figure 29. Test Circuit for Pulse Response

## 10 Detailed Description

### 10.1 Overview

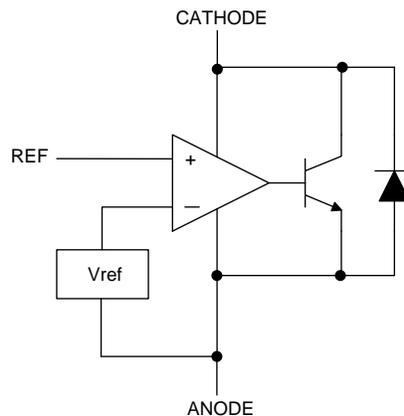
ATL43x is a low power counterpart to TL431 and TLV431, having lower minimum cathode current ( $I_{k(\min)} = 35 \mu\text{A}$  vs 0.1/1.0 mA). Like TL431, ATL43x is used in conjunction with its key components to behave as a single voltage reference, error amplifier, voltage clamp or comparator with integrated reference.

ATL43x can be operated and adjusted to cathode voltages from 2.5 V to 36 V, making this part optimum for a wide range of end equipments in industrial, auto, telecom & computing. In order for this device to behave as a shunt regulator or error amplifier,  $> 35 \mu\text{A}$  ( $I_{\min(\max)}$ ) must be supplied in to the cathode pin. Under this condition, feedback can be applied from the Cathode and Ref pins to create a replica of the internal reference voltage.

Various reference voltage options can be purchased with initial tolerances (at 25°C) of 0.5% and 1.0%. These reference options are denoted by B (0.5%) and A (1.0%) after the ATL43x.

The ATL43xxI devices are characterized for operation from  $-40^\circ\text{C}$  to  $85^\circ\text{C}$ , and the ATL43xxQ devices are characterized for operation from  $-40^\circ\text{C}$  to  $125^\circ\text{C}$ .

### 10.2 Functional Block Diagram



### 10.3 Feature Description

ATL43x consists of an internal reference and amplifier that outputs a sink current based on the difference between the reference pin and the virtual internal pin. The sink current is produced by an internal Darlington pair.

When operated with enough voltage headroom ( $\geq 2.5 \text{ V}$ ) and cathode current ( $I_{kA}$ ), ATL43x forces the reference pin to 2.5 V. However, the reference pin can not be left floating, as it needs  $I_{\text{ref}} \geq 0.1 \mu\text{A}$  (please see the [Functional Block Diagram](#)). This is because the reference pin is driven into an NPN, which needs base current in order operate properly.

When feedback is applied from the Cathode and Reference pins, ATL43x behaves as a Zener diode, regulating to a constant voltage dependent on current being supplied into the cathode. This is due to the internal amplifier and reference entering the proper operating regions. The same amount of current needed in the above feedback situation must be applied to this device in open loop, servo or error amplifying implementations in order for it to be in the proper linear region giving ATL43x enough gain.

Unlike many linear regulators, ATL43x is internally compensated to be stable without an output capacitor between the cathode and anode; however, if it is desired to use an output capacitor [Figure 15](#) through [Figure 22](#) can be used as a guide to assist in choosing the correct capacitor to maintain stability.

## 10.4 Device Functional Modes

### 10.4.1 Open Loop (Comparator)

When the cathode/output voltage or current of ATL43x is not being fed back to the reference/input pin in any form, this device is operating in open loop. With such high gain in this configuration, ATL43x is typically used as a comparator. Due to the integrated reference, the ATL43x allows users to monitor a certain level of a single signal.

### 10.4.2 Closed Loop

When the cathode/output voltage or current of ATL43x is being fed back to the reference/input pin in any form, this device is operating in closed loop. The majority of applications involving ATL43x use it in this manner to regulate a fixed voltage or current. The feedback enables this device to behave as an error amplifier, computing a portion of the output voltage and adjusting it to maintain the desired regulation. This is done by relating the output voltage back to the reference pin in a manner to make it equal to the internal reference voltage, which can be accomplished via resistive or direct feedback.

## 11 Applications and Implementation

### NOTE

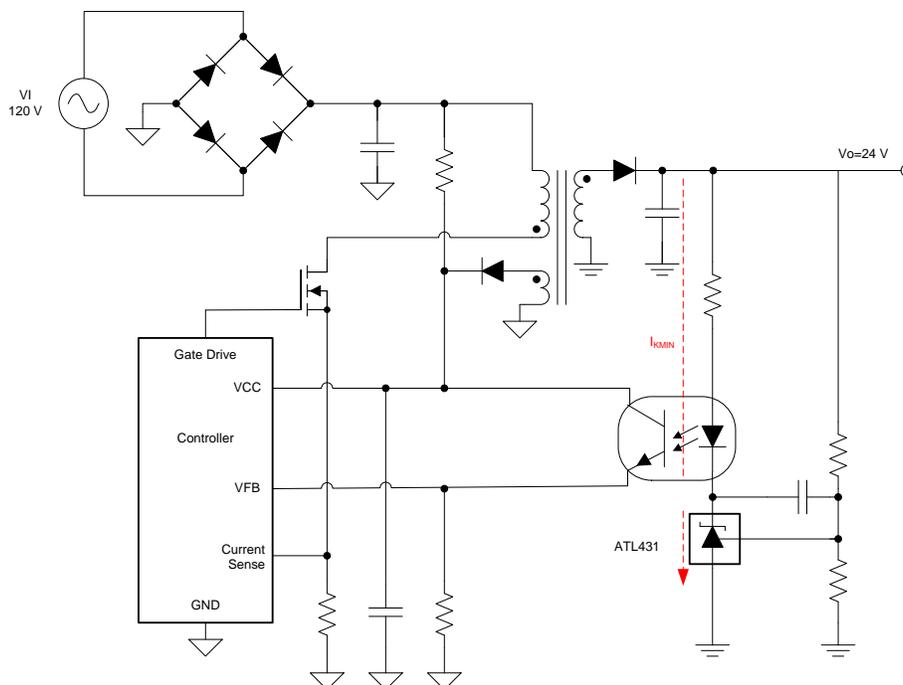
Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 11.1 Application Information

Figure 30 shows the ATL43x used in a 24-V isolated flyback supply. The output of the regulator, plus the forward voltage drop of the optocoupler LED ( $2.5 + 0.7 = 3.2$  V), determine the minimum voltage that can be regulated in an isolated supply configuration. Regulated voltage as low as 5.0 Vdc is possible in the topology shown in Figure 30.

The 431 family of devices are prevalent in these applications, being designers go to choice for secondary side regulation. Due to this prevalence, this section will further go on to explain operation and design in both states of ATL43x that this application will see, open loop (Comparator + Vref) & closed loop (Shunt Regulator).

ATL43x's key benefit in isolated supplies is the no load power savings gained by the  $> 20x$  decrease in  $I_{Kmin}$  from TL431. More information about this and other benefits can be found in the application note *Designing with the "Advanced" TL431, ATL431* [SLVA685](#). Further information about system stability and using a ATL43x device for compensation can be found in the application note *Compensation Design With TL431 for UCC28600*, [SLUA671](#).



**Figure 30. Flyback With Isolation Using ATL43x as Voltage Reference and Error Amplifier**

## 11.2 Typical Applications

### 11.2.1 Comparator with Integrated Reference (Open Loop)

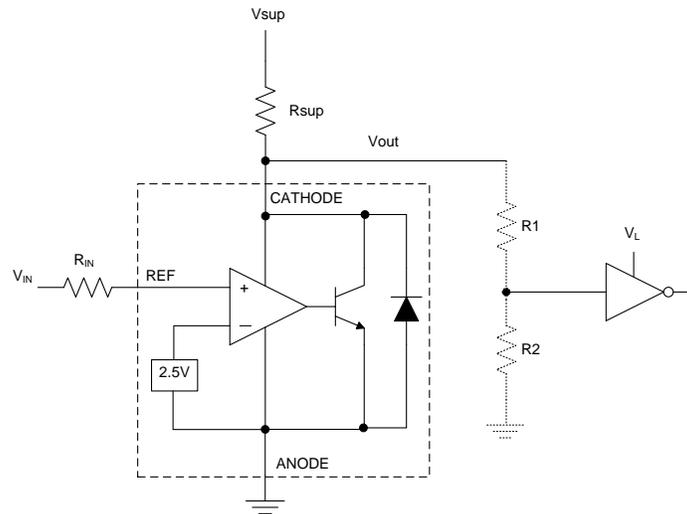


Figure 31. Comparator Application Schematic

#### 11.2.1.1 Design Requirements

For this design example, use the parameters listed in [Table 1](#) as the input parameters.

Table 1. Design Parameters

DESIGN PARAMETER	EXAMPLE VALUE
Input Voltage Range	0 V to 3.3 V
Input Resistance	100 k $\Omega$
Supply Voltage	5 V
Cathode Current ( $I_K$ )	50 $\mu$ A
Output Voltage Level	$\sim 2$ V - $V_{SUP}$
Logic Input Thresholds $V_{IH}/V_{IL}$	1.5 V / 0.8 V

#### 11.2.1.2 Detailed Design Procedure

When using ATL43x as a comparator with reference, determine the following:

- Input voltage range
- Reference voltage accuracy
- Output logic input high and low level thresholds
- Current source resistance

##### 11.2.1.2.1 Basic Operation

In the configuration shown in [Figure 31](#) ATL43x will behave as a comparator, comparing the  $V_{REF}$  pin voltage to the internal virtual reference voltage. When provided a proper cathode current ( $I_K$ ), ATL43x will have enough open loop gain to provide a quick response. With the ATL43x's max Operating Current ( $I_{min}$ ) being 35  $\mu$ A and up to 40  $\mu$ A over temperature, operation below that could result in low gain, leading to a slow response.

### 11.2.1.2.2 Overdrive

Slow or inaccurate responses can also occur when the reference pin is not provided enough overdrive voltage. This is the amount of voltage that is higher than the internal virtual reference. The internal virtual reference voltage will be within the range of  $2.5\text{ V} \pm (0.5\% \text{ or } 1.0\%)$  depending on which version is being used.

The more overdrive voltage provided, the faster the ATL43x will respond.

For applications where ATL43x is being used as a comparator, it is best to set the trip point to greater than the positive expected error (i.e. +1.0% for the A version). For fast response, setting the trip point to  $> 10\%$  of the internal  $V_{\text{ref}}$  should suffice. [Figure 32](#) shows the transition from  $V_{\text{OH}}$  to  $V_{\text{OL}}$  based on the input voltage and can be used as a guide for selecting the overdrive voltage.

For minimal voltage drop or difference from  $V_{\text{in}}$  to the ref pin, it is recommended to use an input resistor  $< 1\text{ M}\Omega$  to provide  $I_{\text{ref}}$ .

### 11.2.1.2.3 Output Voltage and Logic Input Level

In order for ATL43x to properly be used as a comparator, the logic output must be readable by the receiving logic device. This is accomplished by knowing the input high and low level threshold voltage levels, typically denoted by  $V_{\text{IH}}$  &  $V_{\text{IL}}$ .

As seen in [Figure 32](#), ATL43x's output low level voltage in open-loop/comparator mode is  $\sim 2\text{ V}$ , which is sufficient for some  $\geq 5.0\text{ V}$  supplied logic. However, would not work for  $3.3\text{ V}$  and  $1.8\text{ V}$  supplied logic. In order to accommodate this, a resistive divider can be tied to the output to attenuate the output voltage to a voltage legible to the receiving low voltage logic device.

ATL43x's output high voltage is approximately  $V_{\text{sup}}$  due to ATL43x being open-collector. If  $V_{\text{sup}}$  is much higher than the receiving logic's maximum input voltage tolerance, the output must be attenuated to accommodate the outgoing logic's reliability.

When using a resistive divider on the output, be sure to make the sum of the resistive divider ( $R_1$  &  $R_2$  in [Figure 31](#)) is much greater than  $R_{\text{sup}}$  in order to not interfere with ATL43x's ability to pull close to  $V_{\text{sup}}$  when turning off.

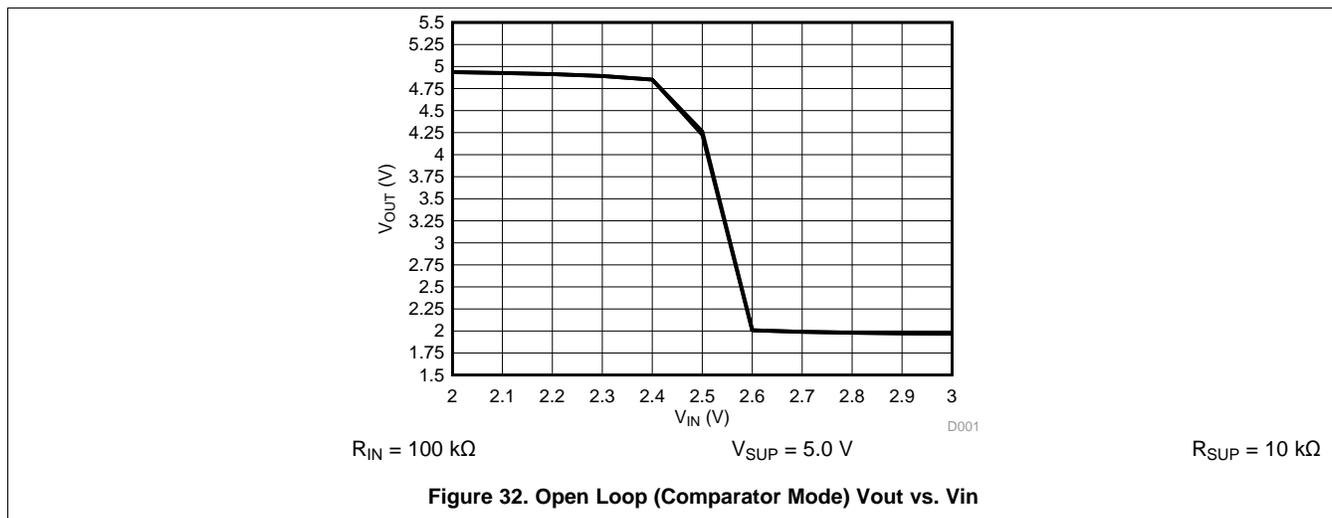
#### 11.2.1.2.3.1 Input Resistance

ATL43x requires an input resistance in this application in order to source the reference current ( $I_{\text{ref}}$ ) needed from this device to be in the proper operating regions while turning on. The actual voltage seen at the ref pin will be:

$$V_{\text{ref}} = V_{\text{in}} - I_{\text{ref}} \times R_{\text{in}} \quad (1)$$

Since  $I_{\text{ref}}$  can be as high as  $0.15\text{ }\mu\text{A}$  it is recommended to use a resistance small enough that will mitigate the error that  $I_{\text{ref}}$  creates from  $V_{\text{in}}$ . Also, the input resistance must be set high enough as to not surpass the absolute maximum of  $10\text{mA}$ .

11.2.1.3 Application Curves



11.2.2 Shunt Regulator/Reference

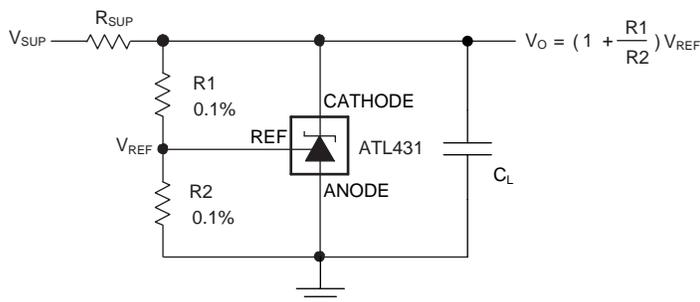


Figure 33. Shunt Regulator Schematic

11.2.2.1 Design Requirements

For this design example, use the parameters listed in Table 2 as the input parameters.

Table 2. Design Parameters

DESIGN PARAMETER	EXAMPLE VALUE
Reference Initial Accuracy	1.0%
Supply Voltage	48 V
Cathode Current (I <sub>k</sub> )	50 μA
Output Voltage Level	2.5 V - 36 V
Load Capacitance	1 nF
Feedback Resistor Values and Accuracy (R1 & R2)	10 kΩ

### 11.2.2.2 Detailed Design Procedure

When using ATL43x as a Shunt Regulator, determine the following:

- Input voltage range
- Temperature range
- Total accuracy
- Cathode current
- Reference initial accuracy
- Output capacitance

#### 11.2.2.2.1 Programming Output/Cathode Voltage

In order to program the cathode voltage to a regulated voltage a resistive bridge must be shunted between the cathode and anode pins with the mid point tied to the reference pin. This can be seen in [Figure 33](#), with R1 & R2 being the resistive bridge. The cathode/output voltage in the shunt regulator configuration can be approximated by the equation shown in [Figure 33](#). The cathode voltage can be more accurately determined by taking in to account the cathode current:

$$V_O = (1 + R1/R2) \times V_{ref} - I_{ref} \times R1 \quad (2)$$

In order for this equation to be valid, ATL43x must be fully biased so that it has enough open loop gain to mitigate any gain error. This can be done by meeting the  $I_{min}$  spec denoted in [Electrical Characteristics, ATL431Ax, ATL432Ax](#) table.

#### 11.2.2.2.2 Total Accuracy

When programming the output above unity gain ( $V_{KA} = V_{ref}$ ), ATL43x is susceptible to other errors that may effect the overall accuracy beyond  $V_{ref}$ . These errors include:

- R1 and R2 accuracies
- $V_{I(dev)}$  - Change in reference voltage over temperature
- $\Delta V_{ref} / \Delta V_{KA}$  - Change in reference voltage to the change in cathode voltage
- $|z_{KA}|$  - Dynamic impedance, causing a change in cathode voltage with cathode current

Worst case cathode voltage can be determined taking all of the variables in to account. Application note [SLVA445](#) assists designers in setting the shunt voltage to achieve optimum accuracy for this device.

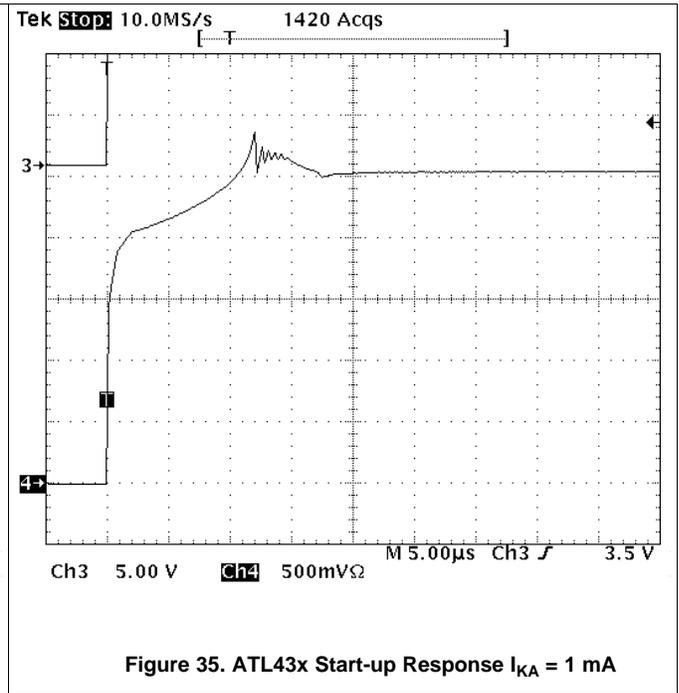
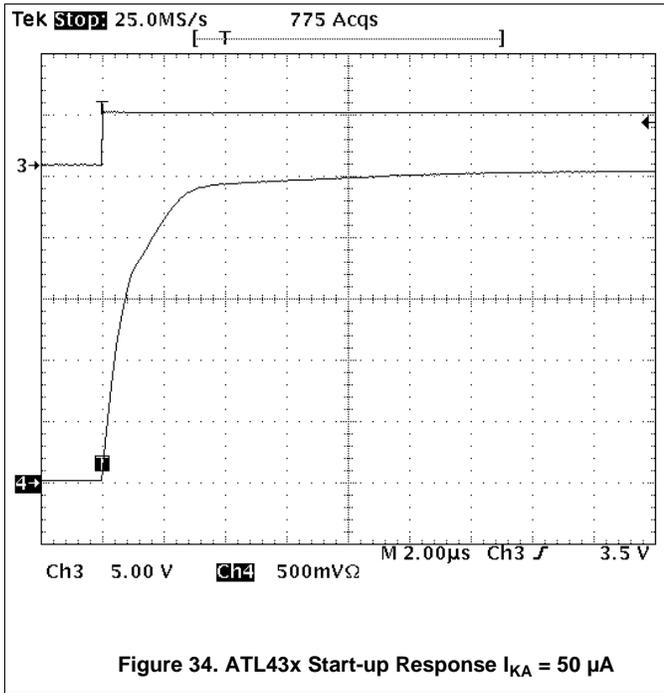
#### 11.2.2.2.3 Stability

Though ATL43x is stable with no capacitive load, the device that receives the shunt regulator's output voltage could present a capacitive load that is within the ATL43x region of stability, shown in [Figure 15](#) through [Figure 22](#). Also, designers may use capacitive loads to improve the transient response or for power supply decoupling.

[Figure 15](#) through [Figure 22](#) should be used as a guide for capacitor selection and compensation. It is characterized using ceramic capacitors with very low ESR. When it is desirable to use a capacitor within the unstable region, higher ESR capacitors can be used to stabilize ATL43x or an external series resistance can be added. For more information and guidance on ESR values, please refer to the application note *Designing with the "Advanced" TL431, ATL431* [SLVA685](#).

Unlike TL431, the stability boundary is characterized and determined with resistors 250Ω and greater. Which is more suitable for low cathode current applications.

11.2.2.3 Application Curves



## 12 Power Supply Recommendations

When using ATL43x as a Linear Regulator to supply a load, designers will typically use a bypass capacitor on the output/cathode pin. Be sure that the capacitance is within the stability criteria shown in [Figure 15](#) through [Figure 22](#).

In order to not exceed the maximum cathode current, be sure that the supply voltage is current limited. Also, be sure to limit the current being driven into the Ref pin, as not to exceed its absolute maximum rating.

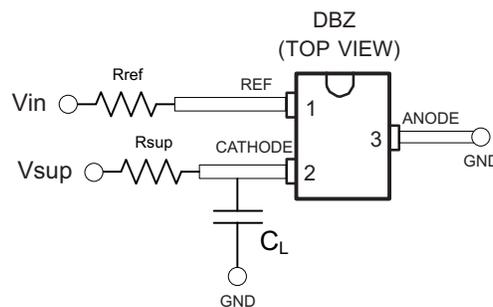
For applications shunting high currents, pay attention to the cathode and anode trace lengths, adjusting the width of the traces to have the proper current density.

## 13 Layout

### 13.1 Layout Guidelines

Place decoupling capacitors as close to the device as possible. Use appropriate widths for traces when shunting high currents to avoid excessive voltage drops.

### 13.2 Layout Example



**Figure 36. DBZ Layout Example**

## 14 Device and Documentation Support

### 14.1 Related Links

The table below lists quick access links. Categories include technical documents, support and community resources, tools and software, and quick access to sample or buy.

**Table 3. Related Links**

PARTS	PRODUCT FOLDER	SAMPLE & BUY	TECHNICAL DOCUMENTS	TOOLS & SOFTWARE	SUPPORT & COMMUNITY
ATL431	<a href="#">Click here</a>				
ATL432	<a href="#">Click here</a>				

### 14.2 Trademarks

All trademarks are the property of their respective owners.

### 14.3 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### 14.4 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 15 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
ATL431AIDBZR	PREVIEW	SOT-23	DBZ	3	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM	-40 to 85	ZCR3	
ATL431AQDBZR	PREVIEW	SOT-23	DBZ	3	3000	TBD	Call TI	Call TI	-40 to 125		
ATL431BQDBZR	PREVIEW	SOT-23	DBZ	3	3000	TBD	Call TI	Call TI	-40 to 125		
ATL432AQDBZR	PREVIEW	SOT-23	DBZ	3	3000	TBD	Call TI	Call TI	-40 to 125		
ATL432BQDBZR	PREVIEW	SOT-23	DBZ	3	3000	TBD	Call TI	Call TI	-40 to 125		

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "-" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

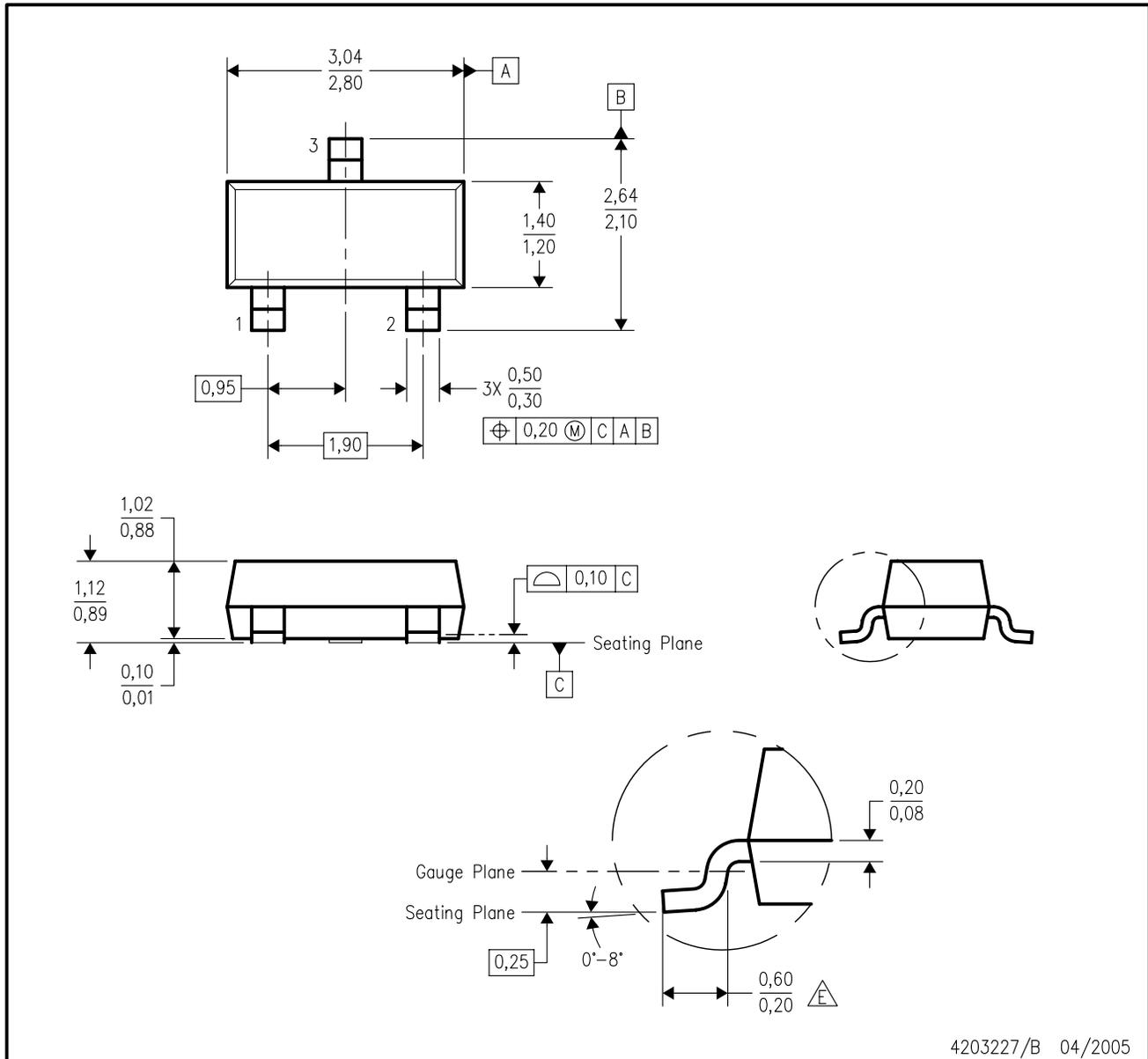
(6) Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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DBZ (R-PDSO-G3)

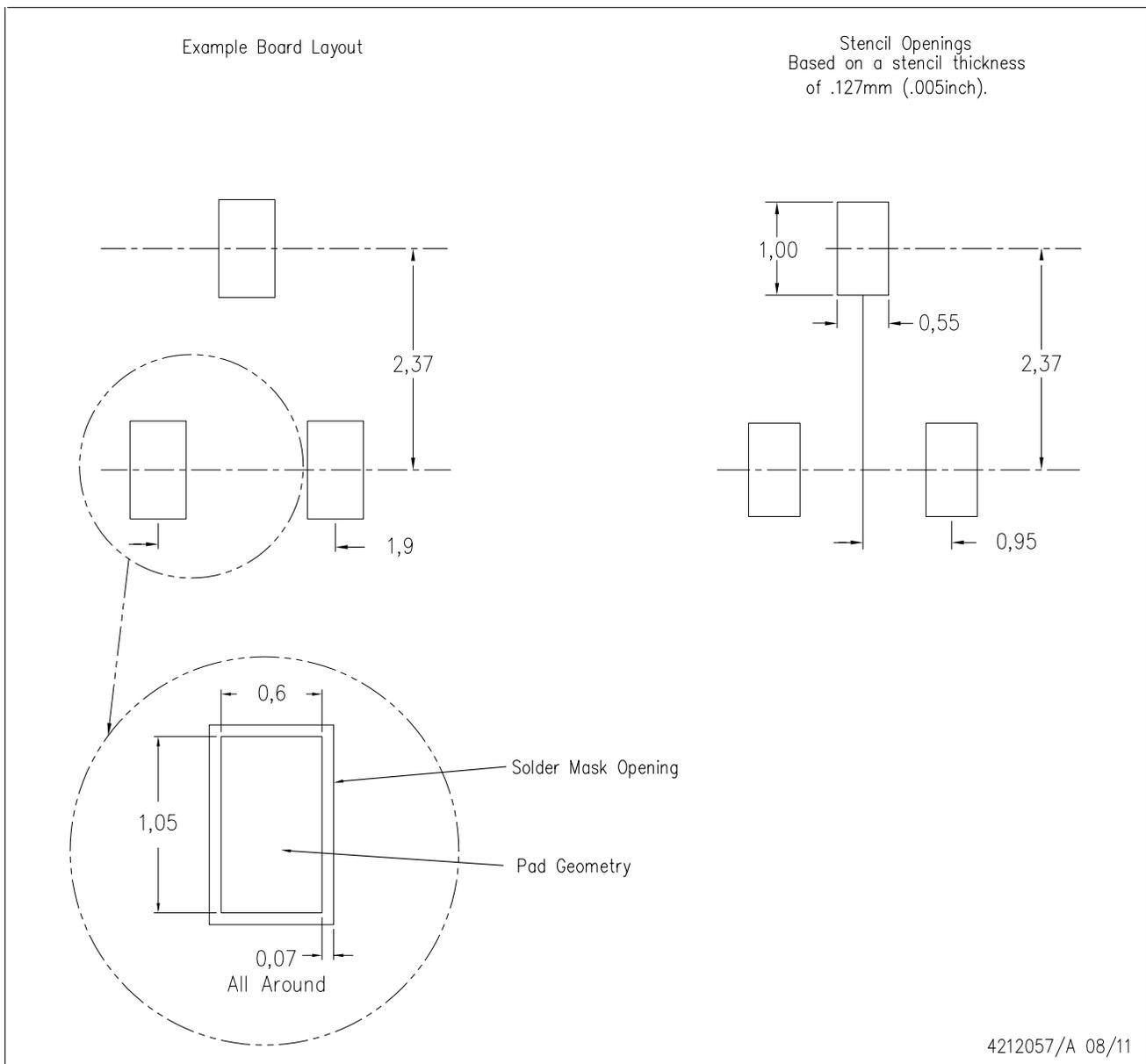
PLASTIC SMALL-OUTLINE



- NOTES:
- A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
  - B. This drawing is subject to change without notice.
  - C. Lead dimensions are inclusive of plating.
  - D. Body dimensions are exclusive of mold flash and protrusion. Mold flash and protrusion not to exceed 0.25 per side.
- Falls within JEDEC TO-236 variation AB, except minimum foot length.

DBZ (R-PDSO-G3)

PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
  - D. Publication IPC-7351 is recommended for alternate designs.
  - E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.

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